

SULPHATION AND CARBONIZATION OF OIL SHALE CFBC ASHES IN HETEROGENEOUS SYSTEMS

R. KUUSIK^{*(a)}, M. UIBU^(a), M. TOOM^(a)
M.-L. MUULMANN^(a), T. KALJUVEE^(a), A. TRIKKEL^(b)

^(a) Laboratory of Inorganic Materials

^(b) Department of Inorganic Chemistry
Tallinn University of Technology,
5 Ehitajate Rd., 19086 Tallinn Estonia

To explain chemical reactivity of oil shale ashes formed in circulating fluidized bed boilers towards SO₂ and CO₂, heterogeneous gas–solid and gas–solid–water model systems were studied. For comparison, the ashes from boilers of pulverized firing were used. The effect of pre-treatment conditions, differences in chemical and phase composition as well as physical properties of the ashes on the binding parameters were estimated.

Introduction

In the course of combustion, fuel inorganic part undergoes several chemical transformations, from decomposition processes to formation of new secondary mineral compounds and phases at higher temperatures. Inorganic matter (about 70% of oil shale mass) of the Estonian oil shale consists mainly of two components: carbonate matter and sandy-clay matter [1].

The mechanism of the processes that take place during pulverized firing (PF) of oil shale is thoroughly examined including the formation of ash deposits at heat-transfer surfaces [1, 2]. Investigations of fly ash composition and reactivity brought about developing and introducing ash-recycling processes like production of various building materials, cement with special properties and other products [3]. Ash is also utilized as an expedient material in road construction as well as soil conditioner in agriculture [4] and neutralizing additive in the production of mineral fertilizers [5]. In addition, it could be used as a SO₂ sorbent [6, 7].

* Corresponding author: e-mail rein.kuusik@ttu.ee

Table 1. Chemical Composition and Physical Properties of CFBC and PF Ashes

Ash	Fraction	Content, %						CO ₂	S _i	S _{Sulphate}	S _{Sulphide}	d _{means} μm	SSA, m ² /g
		CaO _i	CaO _f	MgO _i	CaO _{f,c} *	CaO _i	CO ₂						
CFBC/BA	Initial	49.39	12.48	9.25	37.41	15.14	4.53	4.32	0.10	197	2.06		
	-45 μm	14.79	11.22	32.74	11.22	11.22					4.77		
CFBC/INT	Initial	47.59	18.87	13.65	20.69	1.23	7.76	7.70	0.02	95	2.61		
	-45 μm	18.29	1.62	20.69	1.62	1.62					4.16		
CFBC/ECO	Initial	32.84	10.40	9.50	18.38	5.48	2.32	2.22	0	27	6.89		
	-45 μm	10.58	4.63	17.27	4.63	4.63					7.50		
CFBC/PHA	Initial	35.17	12.26	10.77	18.52	4.30	3.31	3.27	0.0013	32	5.40		
	-45 μm	12.47	4.14	18.51	4.14	4.14					5.89		
CFBC/ESPA1	Initial	29.52	8.45	8.33	14.99	4.60	1.71	1.71	0	25	8.00		
	-45 μm	8.15	3.84	13.56	3.84	3.84					8.63		
CFBC/ESPA4	Initial	28.88	2.82	9.35	7.96	3.80	2.23	2.21	0	23	7.92		
	Initial	33.28	10.33	9.50	19.75	6.41	2.46	2.43	0.03	28	7.11		
CFBC/Mix	-45 μm	9.31	5.57	17.37	5.57	5.57					8.23		
	Initial	50.75	24.84	15.19	29.14	2.75	1.27	1.27	0	115	1.75		
PF/BA	-45 μm	25.92	2.84	30.40	2.84	2.84					2.58		
	Initial	54.71	23.08	7.81	24.53	0.96	1.98	1.93	0	105	0.50		
PF/SHA	Initial	48.00	16.04	8.24	19.71	2.50	2.52	2.52	0.006	53	0.44		
	Initial	49.39	22.52	14.19	23.58	0.70	1.33	1.33	0	48	0.36		
PF/CA	-45 μm	22.79	0.89	24.14	0.89	0.89					1.45		
	Initial	36.08	13.56	11.26	15.21	1.16	2.74	2.74	0	24	0.61		
PF/ESPA1	Initial	26.85	5.98	5.98	7.05	0.80	3.67	3.67	0	23	1.09		
	Initial												

* – calculated on the basis of CO₂ and CaO_f content.

Compared to PF, in the case of circulating fluidized bed combustion (CFBC) operating temperatures are considerably lower. Consequently, chemical and phase composition of CFBC waste ashes differ noticeably [8], and that is why the differences in chemical reactivity can also be expected.

The aim of the current study was to elucidate chemical reactivity of CFBC ashes compared to PF ones in the systems that are important in the formation of ash deposits in a boiler, at ash deposition at landfill, at flue gas desulphurization as well as at reducing CO₂ emissions.

Materials and Methods

Ash samples used were collected from different points of the ash-separation systems of CFBC and PF boilers at the Eesti Thermal Power Plant. The CFBC ashes studied were bottom ash (CFBC/BA), intrex ash (CFBC/INT), economizer ash (CFBC/ECO), air preheater ash (CFBC/PHA), electrostatic precipitator ash from fields 1 and 4 (CFBC/ESPA 1 and 4) and mixture of ashes (CFBC/Mix) taken from a common ash silo where the ash from different units is collected before landfilling on ash fields. The PF ashes used were bottom ash (PF/BA), superheater ash (PF/SHA), economizer ash (PF/ECO), cyclone ash (PF/CA) and electrostatic precipitator ash from fields 1 and 3 (PF/ESPA 1 and 3). Chemical composition and physical properties of these ashes are presented in Table 1 and discussed in more detail in paper [8].

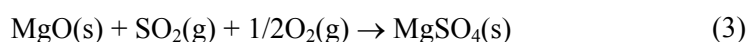
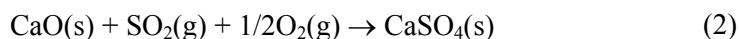
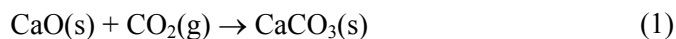
Reactivity of ashes towards SO₂ or CO₂ was tested in a heterogeneous gas-solid system using thermogravimetric equipment (Q-derivatograph, MOM) under isothermal conditions. In both cases the temperature of the isothermal experiment was 700 °C, partial pressure of SO₂ or CO₂ was 190 and 144 mm Hg, respectively. The samples (100 ± 0.5 mg) were heated up to 700 °C in the air with heating rate of 10 K/min. Gas mixture was then fed into the furnace with the rate of 270 ml/min. Thickness of sample layer in multiplate Pt crucibles was about 0.2–0.3 mm. To study the effect of grinding on SO₂ and CO₂ binding, the initial samples (except for CFBC/BA, which was slightly crushed to pass the 630 µm sieve) and the ground ones were used. Samples were ground in an one-ball vibration mill until its most part (approx 85–100%) passed through the 45-µm sieve. In some experiments with CO₂, samples were heated up to 900 °C to achieve full decomposition (FD) of carbonates and then cooled to 700 °C to perform isothermal binding.

To characterize high-temperature binding of SO₂ and CO₂ by ashes, the following parameters were calculated:

- SO₂- or CO₂-binding capacity (*BC*; weight of SO₂ or CO₂ bound by 100 mg of sample),
- SO₂- or CO₂-binding rate (*W*; mg SO₂ or CO₂ per mg sample·min⁻¹),

- SO₂- or CO₂-binding efficiency, (*BE*, %) showing the extent of utilization of CaO and MgO contained in the sample

The parameters were calculated on the basis of experimental and analyses data and the following summary binding reactions:



Carbonization of aqueous suspensions of ash with model gas, whose composition (10% CO₂ and 90% air) simulated CO₂ content of flue gases formed at oil shale combustion, was carried out in an absorber (diameter 55 mm, water column height 500 mm) equipped with magnetic stirrer for achieving a better interfacial contact and a sintered glass gas distributor (pore diameter 100 μm). The experiment was carried out until suspension pH reached 7.5. Then the suspension was filtered and solid residue dehumidified at 105 °C. For the liquid phase, Ca²⁺ content [9], TDS (total dissolved solids) and alkalinity [10] were determined. Content of free CaO [11], pH of aqueous suspension of solid residue [12] and CO₂ were determined in the solid residue.

Results and Discussion

Free CaO is the main binder of SO₂ and CO₂ in the ashes (Reactions (1) and (2)). Although MgO does not take part in CO₂ binding under these conditions [13], it has a certain role in SO₂ binding [13, 14]. Hence, the negative influence of coarser fractional composition of the samples and, correspondingly, the lower level of specific surface area (SSA) in the case of, for example, CFBC/BA (mean particle size 197 μm; SSA 2.1 m²/g) and CFBC/INT (95 μm; 2.6 m²/g) should be compensated by higher level of free CaO content – 11.9 and 18.9%, respectively (see Table 1).

PF/BA and PF/CA are both characterized by a quite high content of free CaO (23–25%), but they differ noticeably (5 times) in their SSA. PF/ESPA1 is characterized by fine fractional composition ($d_{mean} = 24 \mu\text{m}$), low content of free CaO, but despite small particle size by a low value of SSA (0.61 m²/g) and should show a modest binding activity. CFBC/ECO and CFBC/PHA are somewhere in the middle of the scale considering these parameters.

Comparing chemical composition of ground to $-45 \mu\text{m}$ samples and initial samples (see Table 1) one can notice that content of free CaO in initial and ground samples in most cases is similar being slightly higher for ground ones. The difference was 1–10%, except for CFBC/BA (20%). CO₂ content was slightly less in ground CFBC ashes and higher in PF ones. SSA

increased noticeably during grinding for PF/CA, CFBC/BA, CFBC/INT and PF/BA (1.6–4 times). For the other ashes the increase was about 10%.

Transformations in the Gas–Solid System SO₂–Ash

After 30 minutes of the contact between solid and gaseous phases, SO₂-binding capacity of different CFBC ashes was about 26–30 mg SO₂ per 100 mg sample. 55–70% of this value was achieved during the first 2-min contact already (Fig. 1).

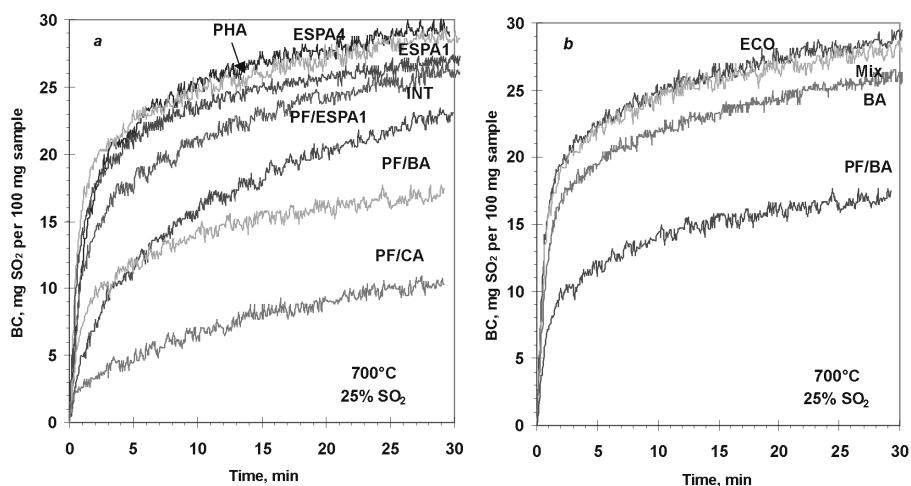


Fig. 1. SO₂-binding capacity (*BC*) of the ashes (for comparison, PF/BA is presented in both diagrams). Pulverized firing ashes marked by PF

BC values for PF ashes differed from each other more considerably – from 10.4 to 23.1 mg SO₂ per 100 mg sample – being the highest for PF/ESPA1. During a 2-min contact, PF/BA bound 58%, while PF/ESPA1 and PF/CA only 33% of the total amount of bound sulphur dioxide. This data correspond to the data obtained in our earlier research [13, 14] and can be explained by the differences in chemical and fractional composition as well as in physical and chemical properties of the ashes. Thus, CFBC/BA and CFBC/INT have coarser fractional composition and lower SSA level, but higher free CaO content, while CFBC/ESPA has fine fractional composition (and high level of SSA), but low content of free CaO (see Table 1). Differences in *BC* values for PF/BA and PF/CA can be explained by their different SSA values (1.75 and 0.36 m²/g, respectively).

During the initial period of the contact (first 30 sec), ECO, PHA, ESPA1 and Mix were the most active among CFBC ashes, having average SO₂-binding rate *W* 0.20–0.23 mg SO₂ per mg sample·min⁻¹. The *W* values for INT, BA and ESPA were 4, 0.16 and 0.13 mg SO₂ per mg sample·min⁻¹, respectively.

In the experiments of SO₂-binding MgO, free CaO and, partially, Ca-silicates can take part in the reactions with SO₂. So, in this case binding efficiency *BE* was calculated on the basis of total content of CaO and MgO in the sample – $BE(CaO \cdot MgO)$. $BE(CaO \cdot MgO)$ values indicated the highest level of utilization of both oxides for ESPA4 (74%) and the lowest for BA and INT – about 41% (Fig. 2) BA was the most active among PF ashes, having an average SO₂-binding rate 0.10 mg SO₂ per mg sample·min⁻¹. Like other indicators of SO₂-binding ability, the values of $BE(CaO \cdot MgO)$ for PF ashes were much less than those for CFBC ashes: 46.9% (the highest) for ESPA1, 25.7% for BA and 15.4% for CA (Fig. 2).

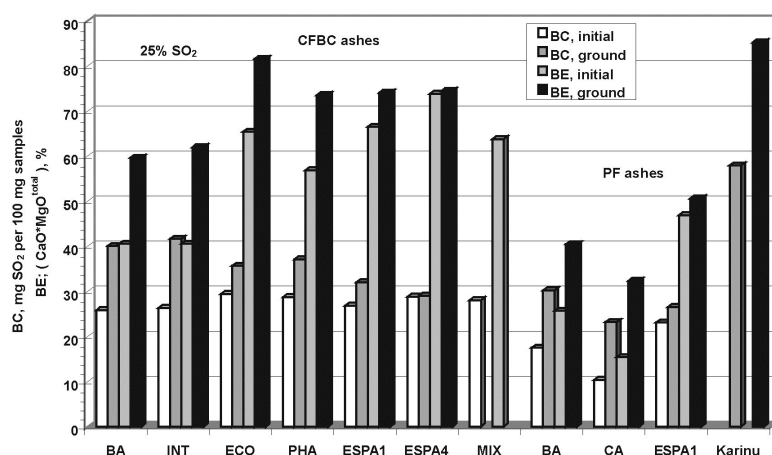


Fig. 2. The influence of grinding on SO₂-binding capacity (*BC*) and efficiency ($BE/CaO \cdot MgO$) at 700 °C after 30-min contact

For all the ashes studied preliminary grinding increased their binding ability. To most extent it was noticed for the ashes characterized by coarse fractional composition (CFBC/BA, CFBC/INT, PF/BA) and/or those having been allocated to high temperatures at PF (especially PF/CA) resulting in the formation of liquid phases hindering further diffusion of SO₂ into the particles.

Thus, grinding increased the *BC* and *BE* values for PF/CA 2.2 times, for CFBC/BA, CFBC/INT and PF/BA 55–70%, for CFBC/ECO and CFBC/PHA 20–30%, for CFBC/ESPA1 and PF/ESPA1 10–20%, and for CFBC/ESPA4 there was no change in these values. Among ground CFBC ashes, *BC* value was the highest for BA and INT (40–42 mg SO₂ per 100 mg sample), *BE* value for ECO – 81.5% (Fig. 2). Among PF ashes, *BC* value was the highest for BA – 30.2 mg SO₂ per 100 mg sample and *BE* value for ESPA1 – 50.6 % (see Fig. 2).

These results are in good correlation with the increase in the SSA of the samples: for PF/CA 4.4 times (from 0.36 m²/g to 1.45 m²/g), for CFBC/BA, CFBC/INT, and PF/BA 1.5–2.3 times, for the other ashes on the level of 1.1

times, except for CFBC/ESPA4 and PF/ESPA1, for which even a small decrease in the SSA was observed. Comparing these results with those obtained with Karinu limestone, the BC values of the more active ashes (CFBC/BA and INT) were only 1.4 times less, but the BE value of CFBC/ECO was on the same level than that of Karinu limestone (see Fig. 2).

An essential increase in the average SO_2 -binding rate in the initial period of the contact was fixed for CFBC/BA and INT – 1.75 and 1.5 times, respectively. But for CFBC/ECO and PHA it was noticeably lower as compared to the initial samples – 75% and 20%, respectively. For PF ashes the average SO_2 -binding rate increased 1.4–2.6 times, being the highest for CA. This phenomena with CFBC/ECO and PHA need an additional study, but it could probably be explained by the negative influence of grinding in the ball mill on structural properties of ashes, for example, the decrease of porosity of the samples or partial closing of the pores on the surface of ash particles.

Transformations in the Gas–Solid System CO_2 –Ash

CO_2 -binding capacities of the ashes stay between 1 and 13 mg $CO_2/100$ mg (Fig. 3). Among CFBC samples, the highest binding capacity was calculated for bottom ash. Binding capacities of ECO, PHA and Mix were about 5 mg $CO_2/100$ mg, the lowest BC values were of INT and ESPA. Bottom ash of pulverized firing bound also about 5 mg of CO_2 per 100 mg sample, binding capacities of PF/CA and PF/ESPA were low.

Grinding of CFBC samples decreased their binding capacities noticeably, except for INT. Decrease in BC was from 12% (BA) to 60–70% (ECO, PHA and ESPA). This phenomenon is specific of CFBC samples, because BC of ground PF samples is about 75–85% higher as compared to the initial ones. This correlates with the increase in specific surface area, which is 4 times higher for ground PF/CA and 1.5 times higher for ground PF/BA. However, grinding increased also SSA of CFBC ashes. The decrease in BC was less for BA and INT, also the increase in SSA during grinding was higher for these samples – 2.3 and 1.6 times, respectively.

Unlike in the reactions with SO_2 , MgO should not take part in CO_2 -binding under these experimental conditions, so, binding efficiency BE was calculated on the basis of the content of free CaO and CaO formed at decomposition of carbonates during heat-up of the samples – $BE(CaO_{fc})$. Besides, recarbonization extent – $X(CO_2)$ as the ratio of the amount of CO_2 bound to the amount present in the sample was used to characterize CO_2 -binding.

The values of binding efficiencies $BE(CaO_{fc})$ reached 40–50% (Table 2), being the highest for the initial samples of CFBC/BA, CFBC/ECO, CFBC/PHA and CFBC/Mix. The changes in binding efficiencies followed the same trend as in the case of binding capacities. They decreased noticeably for the ground CFBC ash samples remaining below 10–20%,

except for BA, and increased for the ground PF ash samples being 40% for PF/BA as compared to 25% for the untreated sample.

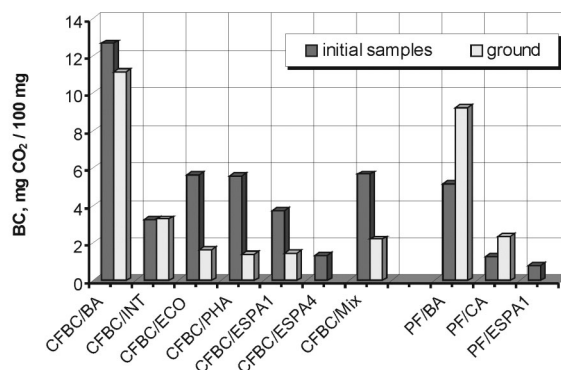


Fig. 3. CO₂-binding capacities (*BC*) of the initial and ground to particle size less than 45 μm ash samples after 30-min binding

Recarbonization extent $X(\text{CO}_2)$ over 100% (see Table 2) indicates that in addition to free CaO formed during decomposition of carbonates at heating, also free CaO present in the initial samples participates in CO₂ binding. $X(\text{CO}_2)$ was high for CFBC/INT (265%) and pulverized firing samples – PF/BA (189%) and PF/CA (181%). High content of free CaO (19–25%) and low (<1%) CO₂ content were specific of these samples. As for the other untreated samples, their $X(\text{CO}_2)$ was in the range of 70–130%. Most probably, the fresh CaO formed during decarbonization at heating is more active in CO₂ binding than the free CaO present in initial samples.

Table 2. $BE(\text{CaO}_f)$ and $X(\text{CO}_2)$ Values of the Initial and Ground Samples, %

Sample	Fraction	$BE(\text{CaO}_f)$	$X(\text{CO}_2)$
CFBC/BA	Initial	52.3	83.7
	-45 μm	48.9	99.4
CFBC/INT	Initial	21.1	265.6
	-45 μm	20.6	203.2
CFBC/ECO	Initial	42.6	103.5
	-45 μm	12.8	35.7
CFBC/PHA	Initial	42.6	130.2
	-45 μm	10.2	34.3
CFBC/ESPA1	Initial	34.5	81.8
	-45 μm	14.4	38.3
CFBC/ESPA4	Initial	23.5	35.1
	-45 μm	23.5	35.1
CFBC/Mix	Initial	42.9	88.6
	-45 μm	17.2	39.7
PF/BA	Initial	25.3	188.8
	-45 μm	39.9	325.3
PF/CA	Initial	7.6	180.7
	-45 μm	12.6	265.4
PF/ESPA1	Initial	7.9	67.9

The effect of pre-treatment and some experiment conditions on binding capacities are presented in Fig. 4. One can see that grinding of CFBC/PHA sample for 30 minutes in the ball mill decreased *BC* from 5.5 to 2.3 mg CO₂/100 mg. The effect of decarbonization temperature is even more severe – the decrease in *BC* for the samples heated before binding to 700 °C and 900 °C (marked by FD) is from 5.5 to 1.8 mg CO₂/100 mg.

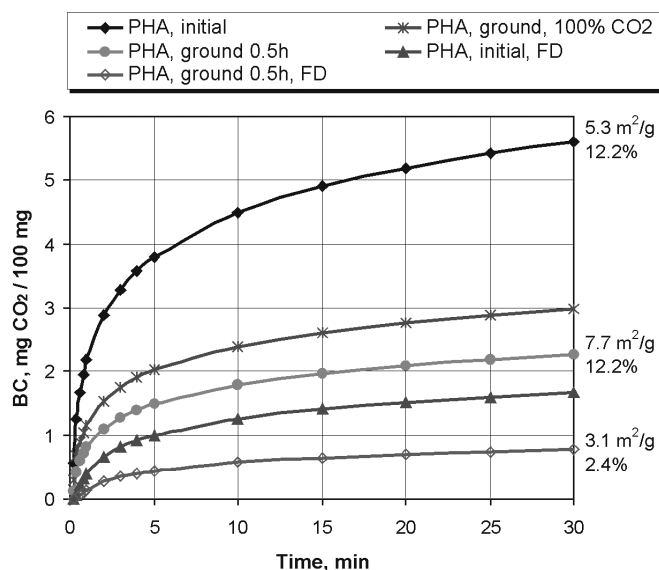


Fig. 4. CO₂-binding capacities of PHA depending on binding duration and pre-treatment conditions. Numbers indicate SSA and CaO_f content before binding

Separate experiments were performed to estimate changes in SSA and CaO_f content during pre-treatment. It can be seen that a 30-min grinding increased SSA from 5.3 to 7.7 m²/g, but heating of this ground sample to 900 °C decreased its SSA to 3.1 m²/g. Also content of free CaO decreased remarkably during heating – from 12.2 to 2.4%. In the samples heated only to 700 °C content of free CaO was 4.8% and SSA of the samples was 10.3 m²/g.

The effect of grinding and decarbonization temperature on *BC* and *BE* needs a more detailed research. Presumably, the decomposition of carbonates and resulting formation of CaO are accompanied by the formation of secondary compounds with free CaO, as noticed earlier [15]. These solid-state reactions taking place during heating of the ash samples of low-temperature CFBC and reducing CaO reactivity could be accelerated in the case of ground samples. Besides, the formation of liquid phases at higher temperatures due to higher content of sulphates, which forms different eutectic mixtures, is possible. It can result in decreasing porosity and increasing diffusion resistance of particles. PF ash samples exposed in boiler to high temperatures and characterized by lower SO₄²⁻ content seem to be more resistant to decarbonization temperature.

Increase in CO₂ concentration from 15 to 100% does not influence *BC* much (see Fig. 4) – the increase in *BC* for the ground sample is about 30%, however, binding rate *W* at the beginning of the process is higher.

Thus, as compared to PF ashes, CO₂ binding capacities of CFBC ashes are 2-3 times higher. The best results were obtained in both cases with

bottom ashes. The method of grinding used improved noticeably binding parameters of PF ashes and reduced those of CFBC ashes. According to the results obtained, it can also be concluded that intensive contamination of heating surfaces in CFB boilers with secondary carbonaceous deposits should not be a serious problem.

CO₂–Ash–Water System

To characterize CO₂-binding in ash–water suspensions the following parameters were used. Carbonization extent was described by index *N* indicating the excess of the CO₂ amount entrained into suspensions over the stoichiometric ratio calculated according to Equation (1). Effectiveness of the carbonization process was described by the CO₂-binding degree (*BD*_{CO₂}). *BD*_{CO₂} shows which part of the theoretical ash-binding capacity is utilized. It was calculated basing on the changes in CO₂ content:

$$BD_{CO_2} = \frac{CO_2}{CO_{2max}} \cdot 100 \quad (\%) \quad (4)$$

where *CO*₂ is analytically determined CO₂ content of the sample, %

*CO*_{2max} is the maximal possible CO₂ content of the sample (%), calculated on the basis of content of free or total CaO in the initial sample as follows:

$$CO_{2max} = \frac{CaO^i \cdot M_{CO_2} / M_{CaO} + CO_2^i}{100 + CaO^i \cdot M_{CO_2} / M_{CaO}} \cdot 100 \quad (5)$$

where *CaO*^{*i*} and *CO*₂^{*i*} denote the content (%) of free or total CaO and CO₂ in the initial sample, respectively.

The results obtained are presented in Table 3 and Figures 5–6. Chemical analysis of the liquid phase indicated that after carbonization the suspensions of both kinds of ashes contain small amounts of alkaline components. In the suspensions of CFBC ashes, content of Ca²⁺ ion is near saturation point or even higher (in the case of intrex ash 1110 mg/l). In the suspensions of PF ashes, the concentrations of Ca²⁺ ions stay on a noticeably lower level (240–590 mg/l). The TDS values were proportional to the content of Ca²⁺ ion.

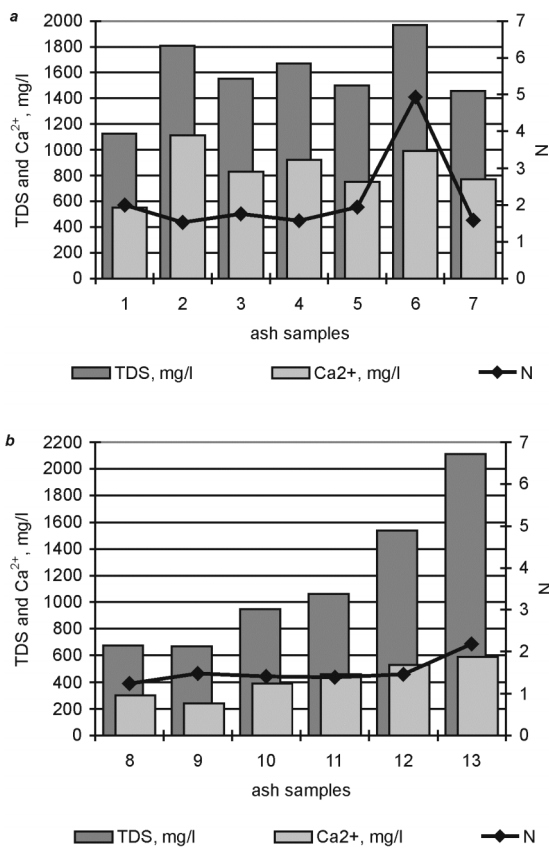
Compared to PF ashes, CFBC ashes can be carbonized more deeply accompanied by lowering of pH of the solid residue in most cases below 9 (with the exception of CFBC/BA, full carbonization of which is inhibited due to coarse fractional composition, see Table 1). Higher pH value (10.9–11.9) is elicited by higher content of free CaO (0.57–3.47%) in solid residues of carbonized PF ashes. Apparently, in the case of PF ashes as nonporous materials some part of free CaO present is not accessible and therefore cannot take part in reaction under these conditions. The content of CO₂ is proportional to that of free CaO and CO₂ in the initial samples (see Table 1).

Table 3. Characterization of Carbonized Ashes

Ash type	CO ₂ , %	CaO _f , %	BD _{CO₂} , %	BD _{CO₂} ^{*1} , %	pH ^{*2}	N	$\frac{m^3CO_2}{t_ash}$
CFBC/BA	23.29	0.88	104.1	59.93	11.55	2.00	944.44
CFBC/INT	15.51	0.43	110.92	55.17	9.6	1.53	1152.77
CFBC/ECO	14.17	0.21	112.28	56.98	8.85	1.76	731.53
CFBC/PHA	14.30	0.22	112.97	57.15	9.33	1.57	759.31
CFBC/ESPA1	12.68	0.18	120.31	56.20	7.24	1.94	652.78
CFBC/ESPA4	11.26	0.12	191.32	52.15	7.43	4.94	555.55
CFBC/Mix	16.09	0.20	119.75	62.34	8.93	1.58	652.78
PF/BA	19.46	1.41	104.45	64.01	11.55	1.24	1229.17
PF/SHA	18.99	1.79	117.49	61.79	11.88	1.48	1361.11
PF/ECO	13.4	3.47	99.92	45.89	11.88	1.41	902.78
PF/CA	17.18	0.61	109.92	60.36	10.88	1.39	1250.83
PF/ESPA1	12.96	0.75	121.39	56.37	10.98	1.46	791.67
PF/ESPA3	7.62	0.57	145.09	42.14	10.95	2.19	523.19

*1 - CO₂-binding degree calculated on the basis of total CaO in initial sample.

*2 - pH of aqueous suspension of solid residue.



Binding degrees that were calculated basing on content of free CaO in the initial samples were in CFBC and PF ashes predominantly over 100% (104.1–191.32% and 99.92–145.09%, respectively) because there can be other CO₂-binding compounds (MgO, Ca-silicates) present in oil shale ash of heterogeneous composition. In general, for total utilization of free CaO the CFBC ashes need less CO₂ per tonne of ash as they contain less free CaO in the initial ash.

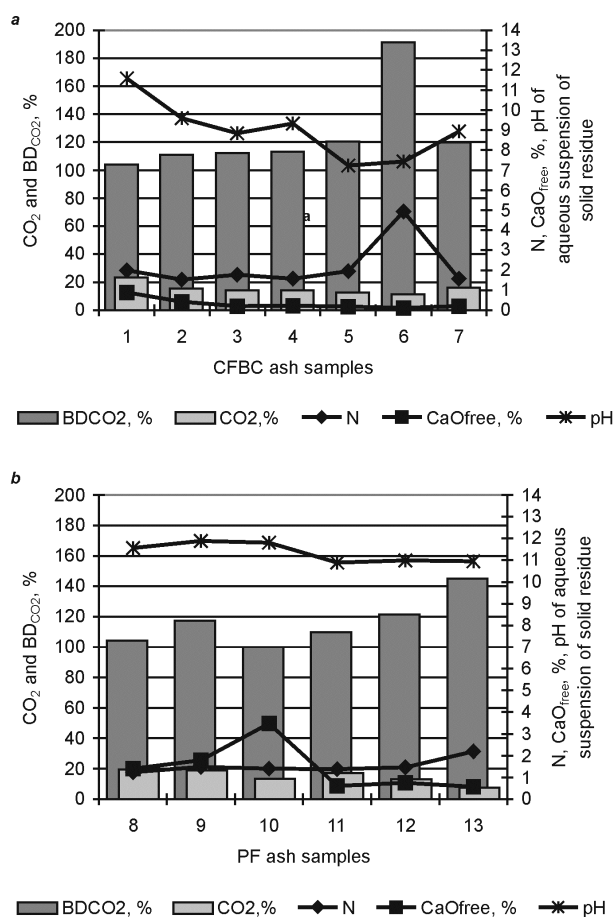


Fig. 6. Characteristics of carbonization process and its final product for CFBC (a) and PF (b) ashes.

1 – CFBC/BA,
 2 – CFBC/INT,
 3 – CFBC/ECO,
 4 – CFBC/PHA,
 5 – CFBC/ESPA1,
 6 – CFBC/ESPA4,
 7 – CFBC/Mix,
 8 – PF/BA,
 9 – PF/SHA,
 10 – PF/ECO,
 11 – PF/CA,
 12 – PF/ESPA1,
 13 – PF/ESPA3

Conclusions

1. Oil shale ashes formed in boilers operating at different combustion technologies differ by their chemical reactivity towards acidic gases.
2. Sulphation of ashes in model conditions shows that SO₂-binding capacity of CFBC ashes at enhanced temperature (700 °C) remained within a narrow range of 26–30 mg (0.41–0.47 mmoles) of SO₂ per 100 mg sample, and in the case of PF ashes between 10 and 27 mg SO₂ per

100 mg sample, being the highest for PF/BA. Grinding of coarser ashes increased their *BC* values noticeably (60–120%). For the other kinds of ashes the increase remained on the level of 15–30%. Consequently, SO₂-binding capacity of CFBC as well as of PF ashes is not completely utilized. Being characterized by a higher binding rate during the initial stage of gas–solid contact, CFBC ashes could be more promising as potential SO₂ sorbents for desulphurization processes of flue gases.

3. Transformations in the gas–solid system CO₂–ash which are important also in evaluating the possibilities for formation of calcareous precipitations on heat transfer surfaces in boilers, especially the recarbonization process of ashes, were investigated. CO₂-binding ability of the ashes at 700 °C was relatively low – in the range of 0.02–0.30 mmols of CO₂ per 100 mg sample being 2-3 times higher for CFBC ashes. Within 30 minutes 8–52% of free CaO present in the sample was utilized. According to these data intensive formation of secondary carbonaceous precipitations on the heat transfer surfaces of the CFB boiler is not foreseen.
4. The results of the experiments on binding gaseous CO₂ by ash–water suspension indicated that in the same conditions, CFBC ashes can be carbonized more intensively and deeply than PF ashes. Besides lime as a compound of the highest reactivity towards CO₂ also other components like MgO and Ca-silicates present in ash take part in CO₂-binding reactions. Owing to improved CO₂-binding rate, more intensive natural CO₂-mineralization of CFBC ashes as compared to PF ashes in open-air deposits as well as intensive binding of CO₂ from flue gases by aqueous suspension of ash are expected.

Acknowledgements

Authors express their gratitude to AC Narva Power Plants Ltd. and Estonian Science Foundation (Grant No. 6195) for financial support and to Dr Helgi Veskimäe for help by carrying out chemical analyses.

REFERENCES

1. *Ots, A.* Oil Shale Combustion Technology. Tallinn, 2004. 768 pp. [in Estonian]
2. *Ots, A., Arro, H., Jovanovic, L., et al.* The Behaviour of Inorganic Matter of Solid Fuels during Combustion. Fouling and Corrosion in Steam Boilers. Beograd, 1980. 276 pp.
3. *Kikas, V.* Composition and binder properties of Estonian kukersite oil shale ash // International Cement-Lime-Gypsum. 1997. Vol. 50, No. 2. P. 112–126.

4. *Kärblane, H.* Handbook of Plant Nutrition and Fertilization. Ministry of Agriculture of the Republic of Estonia. Tallinn, 1996. 285 pp. [in Estonian].
5. Certificate of Authorship 280493 (USSR). Method of Neutralization of Phosphoric Acid / Tallinn Technical University. Veiderma, M. A., Vendelin, A. G., Kuusik, R. O., Kuusk, A. A.-M. Appl. 30.12.1968, No.1293097/23-26. Publ. in B. I., 1970 No.28. MKI C 05b 1/02. [in Russian].
6. *Kuusik, R., Kaljuvee, T., Trikkel, A., Maarend, J., Roundyguine, J.* Dry desulphurization of flue gases by Estonian lime-containing materials // Proc. 10th World Clean Air Congr., Espoo, Finland, May 28–June 2, 1995. Helsinki, 1995. Vol. 1. P. 037.
7. *Trikkel, A.* Estonian Calcareous Rocks and Oil Shale Ash as Sorbents for SO₂ / Academic Dissertation, Tallinn University of Technology: TTU Press, 2001. 70 pp.
8. *Kuusik, R., Uibu, M., Kirsimäe, K.* Composition and physico-chemical characterization of oil shale ashes formed at industrial scale boilers with CFBC // Oil Shale. 2005. Vol. 22, No. 4S. P. 407–419.
9. *Vilbok H., Ott, R.* Volumetric Analysis. Instructions for Practical Works / Tallinn Polytechnical Institute. – Tallinn, 1977. [in Estonian]
10. Water Quality. Determination of Alkalinity. International standard ISO 9963-1:1994(E). lubja määramise me
11. *Reispere, H. J.* Determination of Free CaO Content in Oil Shale Ash / Tallinn Polytechnical Institute. – Tallinn 1966. No 245. P 73–76. [in Estonian]
12. Regulation (EC) No 2003/2003 of the European Parliament and of the Council on October 13, 2003 relating to fertilisers / Official Journal of the European Union. P. 60.
13. *T. Kaljuvee, T., Trikkel, A., Kuusik, R.* Decarbonization of natural lime-containing materials and reactivity of calcined products towards SO₂ and CO₂ // J. Therm. Anal. Cal. 2001. Vol. 64. P. 1229–1240; Proc. 12th Int. Congr. on Thermal Analysis and Calorimetry, Copenhagen, Denmark, Aug. 14–18, 2000. Budapest: Akadémiai Kiadó, 2001. Vol. 3. ISBN 963–05–7791–7. P. 1229–1240.
14. *Kaljuvee, T., Kuusik, R., Trikkel, A., Bender, V.* The role of MgO in the binding of SO₂ by lime-containing sorbents // J. Therm. Anal. Cal. 2005. Vol. 80. P. 591–597.
15. *Kuusik, R., Paat, A., Veskimäe, H., Uibu, M.* Transformations in oil shale ash at wet deposition // Oil Shale. 2004. Vol. 21, No. 1. P. 27–42.

Received June 1, 2005